



ORION EXPLORATION MISSION ENTRY INTERFACE TARGET LINE

JEREMY REA

NASA JOHNSON SPACE CENTER

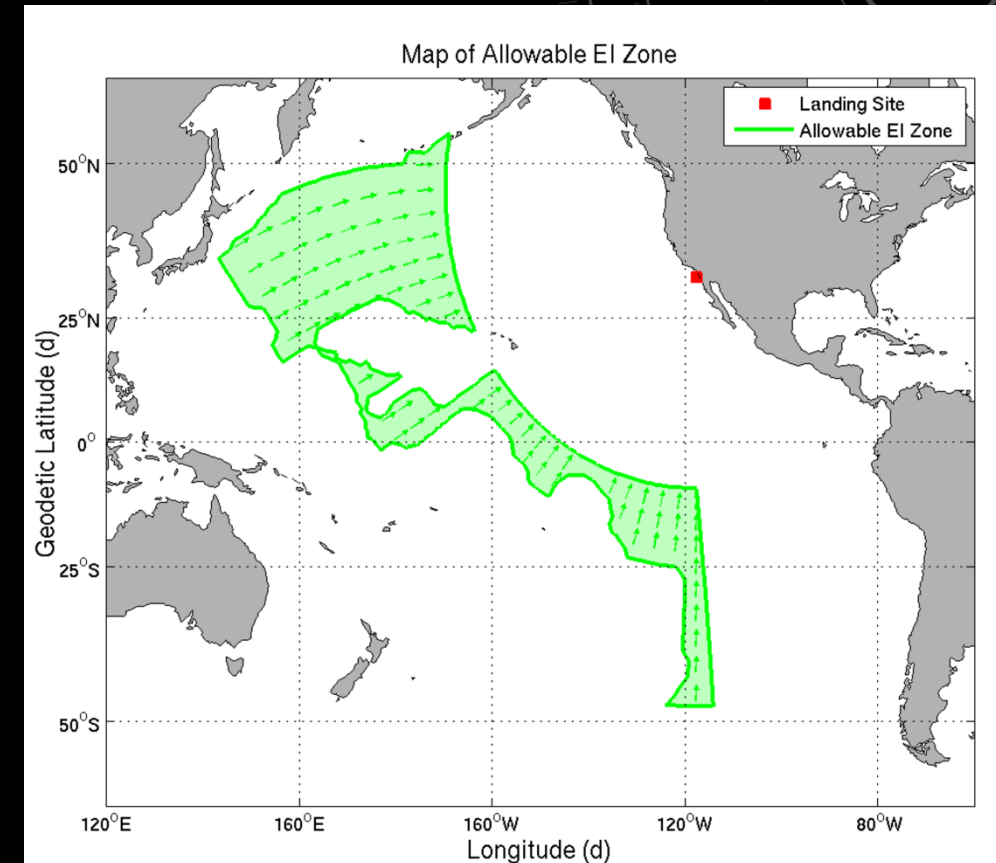
26TH AAS/AIAA SPACE FLIGHT MECHANICS MEETING

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ORION ENTRY CORRIDOR CONSTRAINTS

- Horizontal Constraints
 - Return to San Diego landing zone anytime during the month
 - Preserve weather divert capability to fly up to 1200 nmi short of target
 - Minimum flyable range of 1300 nmi defined by maximum acceleration
 - Dispose of Service Module debris over open ocean
 - Point toward landing site within crossrange capability of vehicle
 - No retrograde entries
- Vertical Constraints
 - Preserve ballistic entry downmode option
 - Stay within heat shield design limits
 - Provide survivable entry for all Earth return scenarios (26 to 36 kft/s)

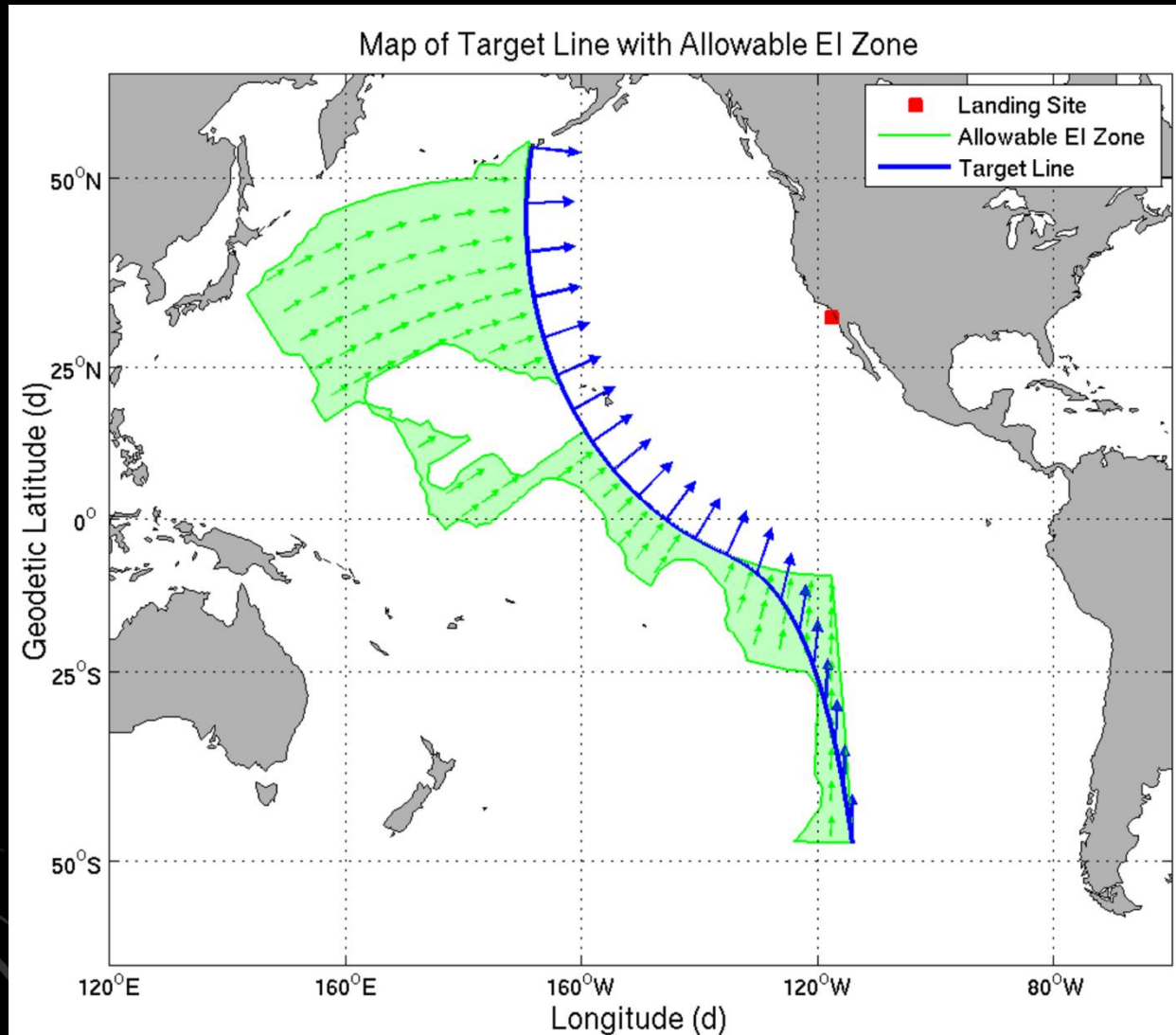


TARGET LINE CRITERIA

- Minimize the range-to-target when possible
- Choose flight path angle to limit ballistic lofting
- Continuously differentiable
- Functionalized target line in form of polynomial

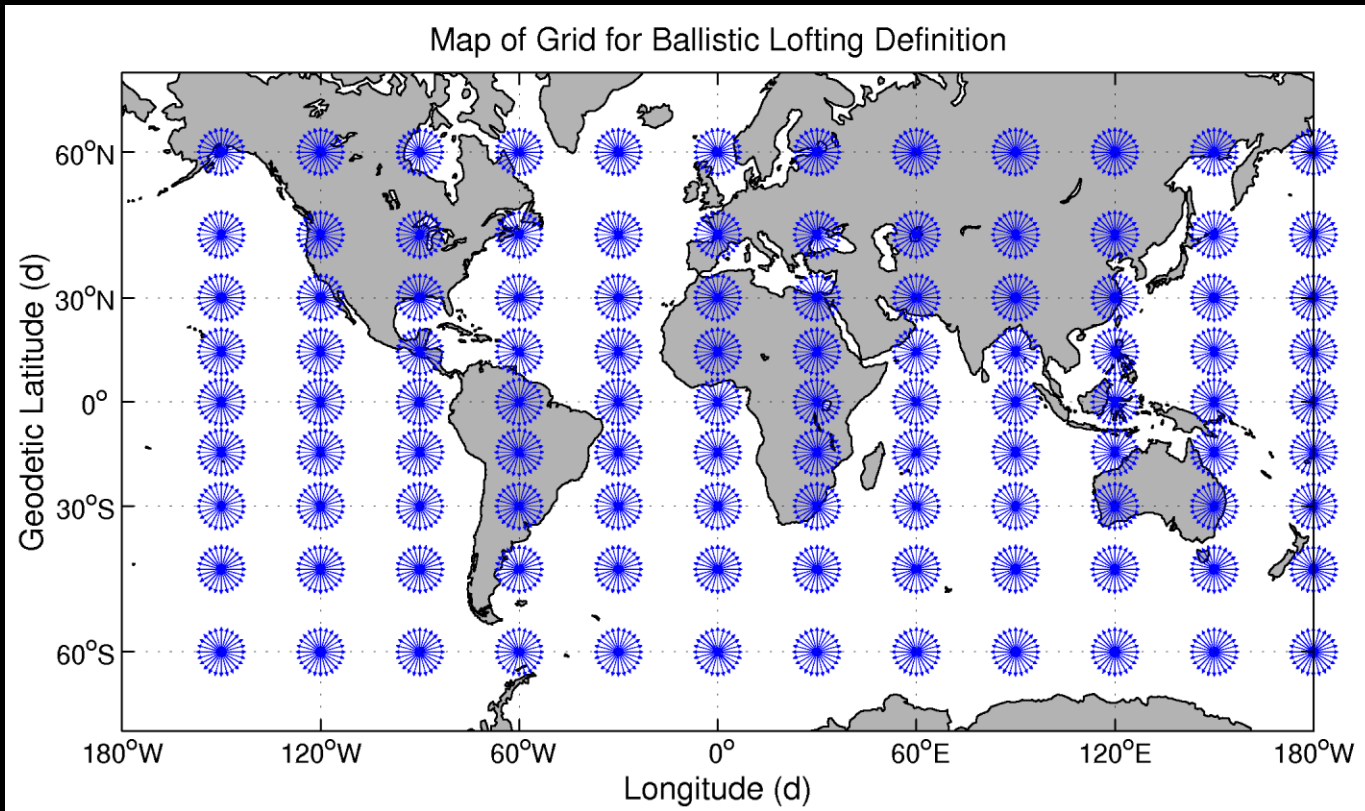


HORIZONTAL TARGET LINE DEFINITION



- Spans entire latitude space
- Follows 2500 nmi arc when possible
- No discontinuities
- Invalid zone between 14° and 21.9° latitude

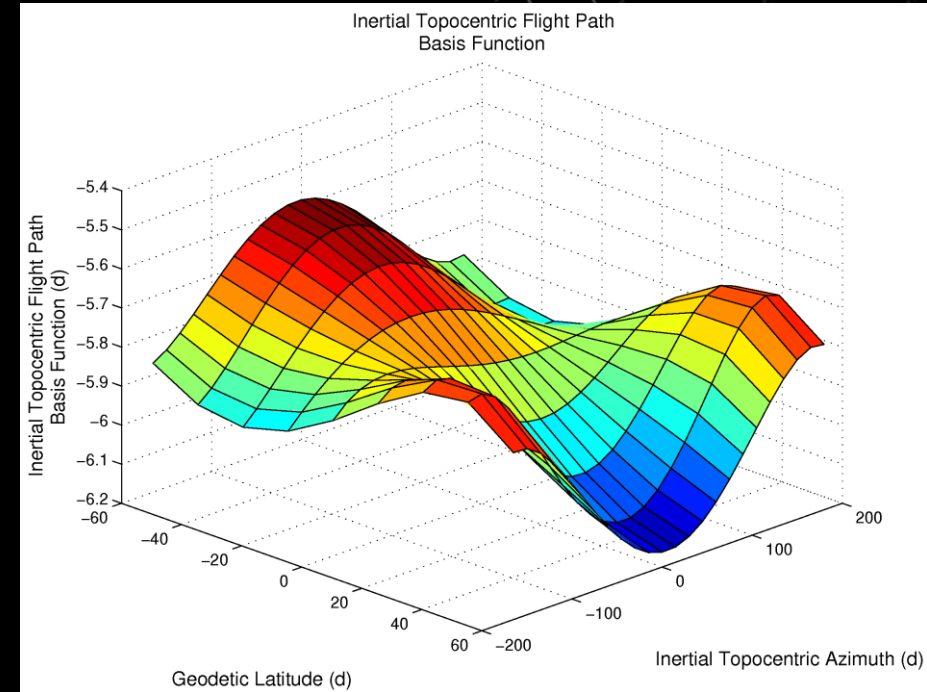
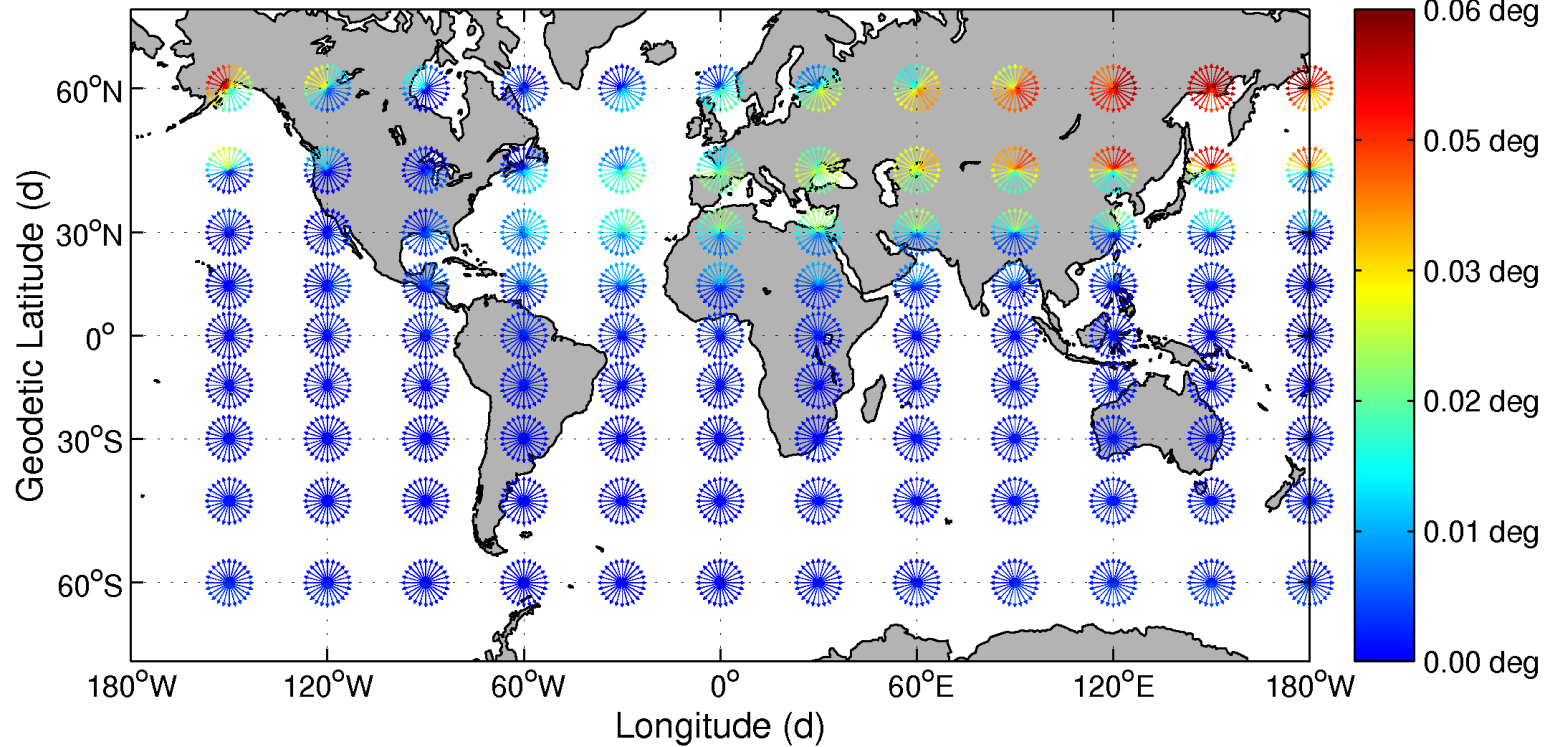
VERTICAL TARGET LINE DEFINITION



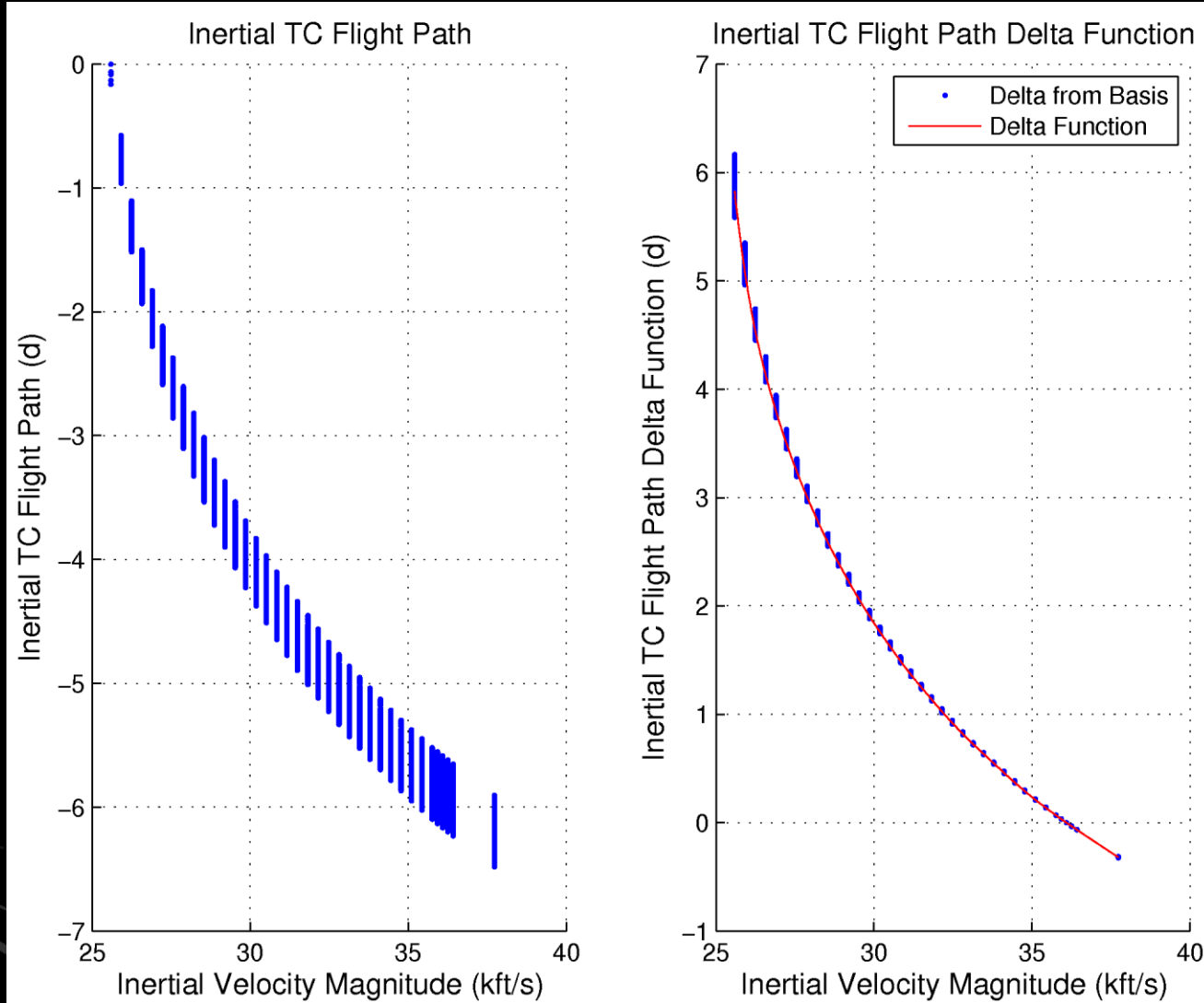
- Define flight path angle that limits ballistic lofting
- Function of:
 - Geodetic latitude
 - Longitude
 - Azimuth
 - Speed

REMOVING DEPENDENCE ON LONGITUDE

Ballistic Lofting Data Relative to Min Value Across Longitude



DEPENDENCE ON SPEED



- Delta function approximates the change in ballistic lofting flight path angle with respect to speed

FUNCTIONALIZATION IN ONE DIMENSION

- Lagrange interpolating polynomial

$$y(x) = \sum_{j=1}^N y_j \phi_j(x)$$

$$\phi_j(x) = \prod_{\substack{m=1 \\ m \neq j}}^N \frac{(x - x_m)}{(x_j - x_m)}$$

$y(x)$ = Approximating polynomial
 N = Number of nodes
 y_j = Value of y at x_j
 $\phi_j(x)$ = Set of interpolating functions

- Optimal node spacing at roots of orthogonal polynomials

$$X_{CGLj} = \cos\left(\frac{(j-1)\pi}{N-1}\right), j = 1, 2, \dots, N$$

(Chebyshev-Gauss-Lobatto Points)

- Mapping to real domain

$$x_j = \frac{(x_N - x_1)X_{CGLj} + (x_N + x_1)}{2}$$

x_j = j^{th} real EI target line parameter
 X_{CGLj} = j^{th} X_{CGL} node point

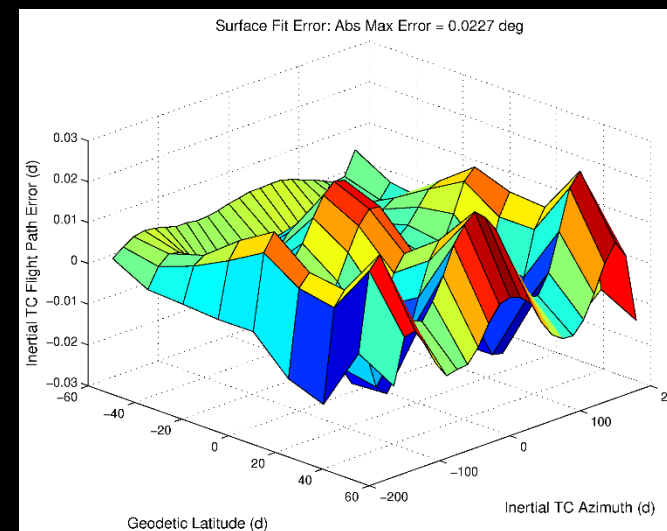
FUNCTIONALIZATION IN TWO DIMENSIONS

- Multivariable Polynomial in Two Variables

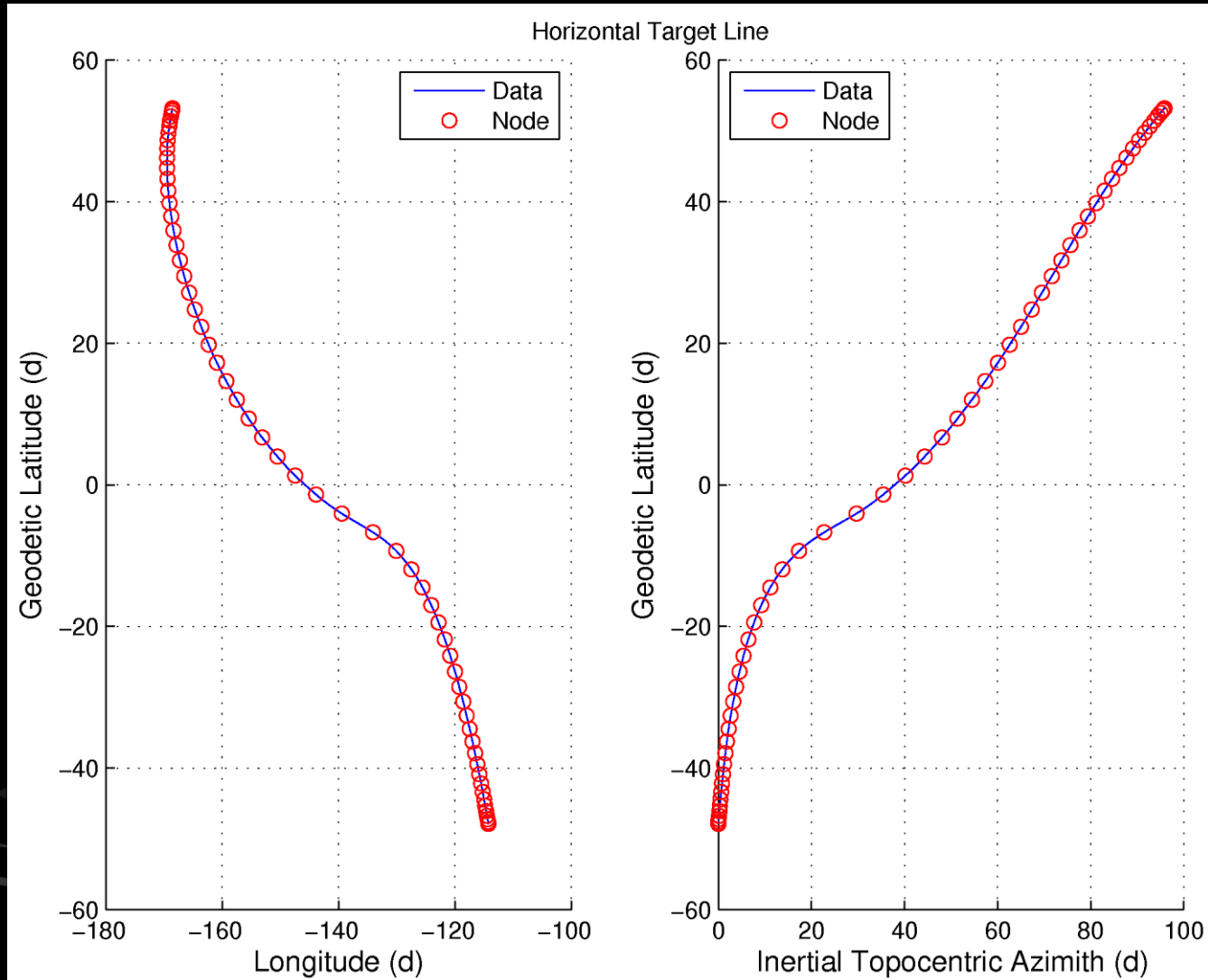
$$z(x, y) = \sum_{i=1}^{N_x+1} \sum_{j=1}^{N_y+1} C_{i,j} x^{(i-1)} y^{(j-1)}$$

$z(x, y)$ = Approximating polynomial
 N_x = Highest order of x
 N_y = Highest order of y
 $C_{i,j}$ = Coefficient i, j

- Flight path angle basis function is fit to this curve using non-constrained optimizer to minimize the norm of the error



HORIZONTAL TARGET LINE

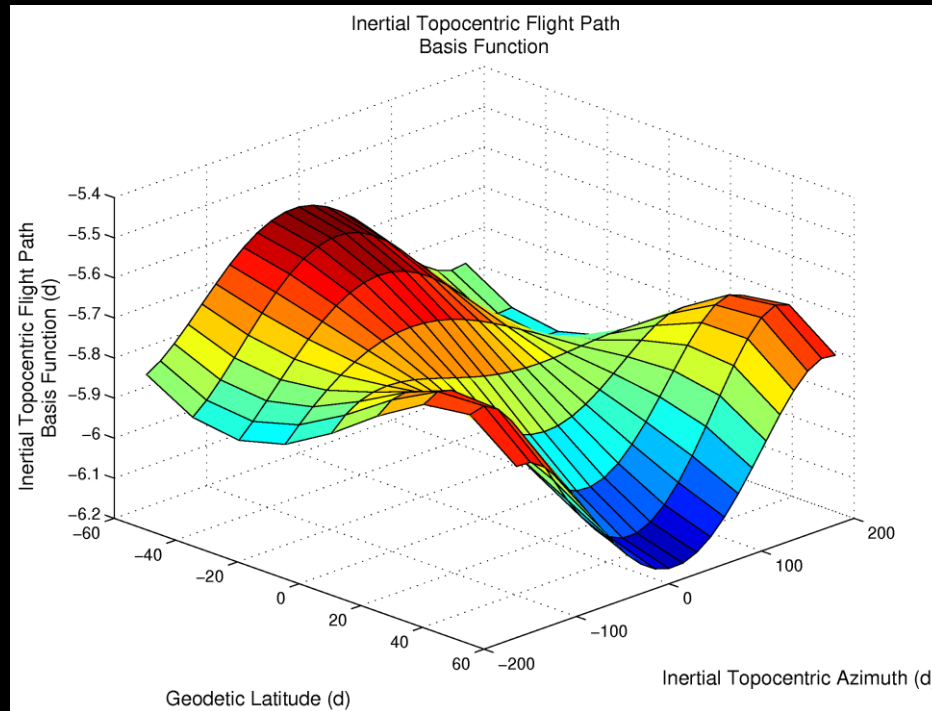


- Independent variable
 - Geodetic latitude
- Dependent variables
 - Longitude
 - Inertial topocentric azimuth
- Lagrange polynomials with 60 nodes

VERTICAL TARGET LINE

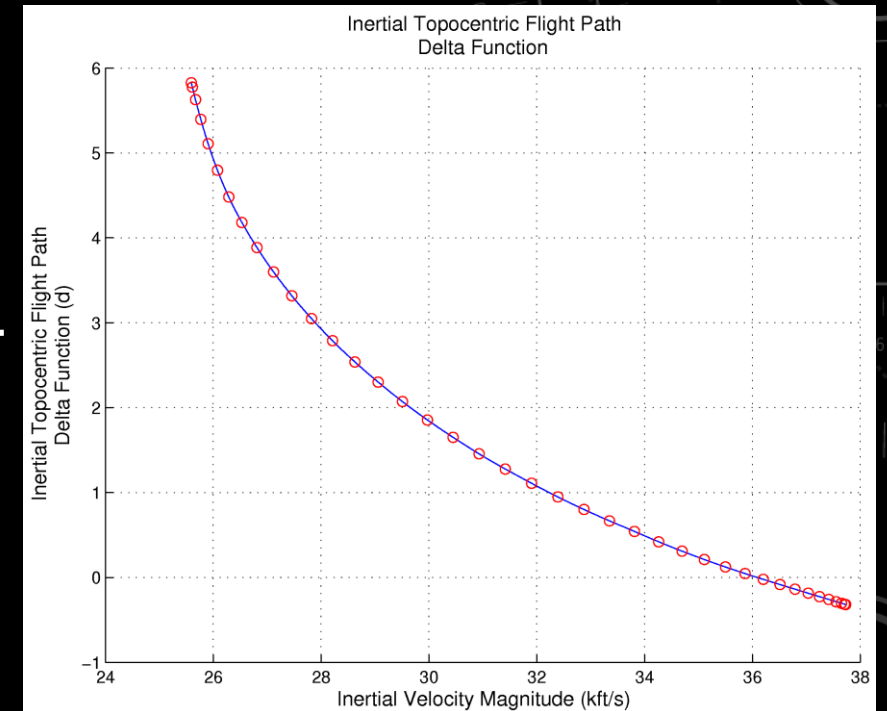
Flight Path Angle (FPA) =

Basis Function: *Ballistic lofting FPA at 36 kft/s*



- Multivariable polynomial of order 4,4
- Independent Variables:
 - Geodetic latitude
 - Inertial topocentric azimuth

Delta Function: *Difference due to speed*



- Lagrange polynomial with 40 nodes
- Independent Variable:
 - Inertial velocity magnitude

SUMMARY

- El target line functionalizes complex set of entry constraints into a set of polynomials
- These polynomials will be used for both on-board targeting and ground-based trajectory planning